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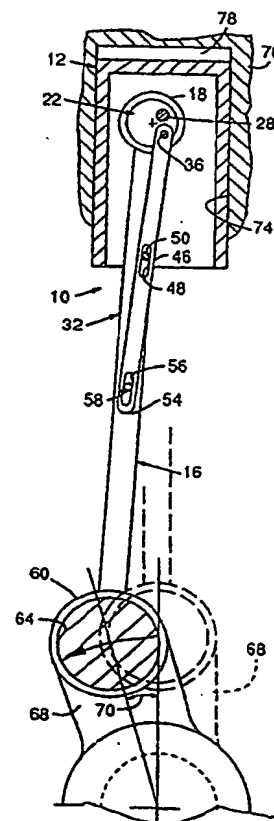
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(21) International Application Number: PCT/US93/08811 (22) International Filing Date: 20 September 1993 (20.09.93) (71)(72) Applicant and Inventor: ROUTERY, Edward, E. [US/US]; 6209 East McKellips, Mesa, AZ 85205 (US). (74) Agent: NISSLE, Tod, R. ; 7150 East Camelback Road, Suite 245, Scottsdale, AZ 85251 (US).		(81) Designated States: AU, BR, CA, CZ, HU, JP, KP, KR, PL, RU, SK, UA, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report.</i>

(54) Title: VARIABLE LENGTH CONNECTING ROD FOR INTERNAL COMBUSTION ENGINE

(57) Abstract

An adjustable length connecting rod assembly (10) for an internal combustion engine (76) provides prolonged periods of substantially constant combustion chamber volume. A rotatable disk (22) mounted in the upper sleeve end (20) of a connecting rod (16) has an eccentric bore (26) for receiving the wrist pin (28) of a piston (12). Another eccentric bore (40) in the disk (22) pivotally receives an upper end of a rigid shifter bar (32). An intermediate portion of the bar (32) is slidably attached to a pin (50) mounted to a lower portion of the piston (12) and a lower portion of the bar (32) is slidably attached to a pin (58) mounted to an intermediate portion of the rod (16). Angular movement of the rod (16) relative to the pin (58) causes the bar (32) to rotate the disk (22), extending or retracting the piston (12) relative to the rod (16).



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- 1 -

VARIABLE LENGTH CONNECTING ROD FOR INTERNAL
COMBUSTION ENGINE

TECHNICAL FIELD

5 This invention relates to internal combustion engines, Stirling engines, compressors, pumps and other apparatus having reciprocating pistons. More particularly, the invention relates to a piston connecting rod assembly as
10 disclosed in applicant's Patent Application Serial No. 07/530,754, filed May 30, 1990, now issued as U. S. Patent No. 5,156,121.

BACKGROUND OF THE ART

15 The apparatus disclosed herein is essentially an improvement to applicant's piston connecting rod assembly indicated above, the entirety of which is incorporated herein by reference.

The prior application discloses an apparatus for providing constant volume combustion (CVC) in a two-stroke or four-stroke internal combustion engine. With constant
20 volume combustion, the entire fuel-air mixture burns before the piston makes any substantial movement downward. Without CVC, a portion of the fuel remains unburned until after the piston has moved a distance downward. This remaining
25 portion of the combustion produces less mechanical work and greater exhaust waste heat, worsening efficiency and thermal concerns. In addition, without CVC some fuel may not be completely burned, resulting in higher concentrations of hydrocarbons, carbon monoxide and other undesirable
30 pollutants in the exhaust gas. The emission problems due to the late or incomplete burning of fuel in a non-CVC engine are worsened by the fact that the expansion of the combustion chamber cools the gases contained therein due to the ideal gas law, further slowing the rate of combustion and delaying the combustion of remaining fuel.
35

Normally, in a conventional piston engine, the piston follows a sinusoidal path as the crank shaft rotates. Thus, the piston is stationary only momentarily

- 2 -

when at top dead center (TDC) and bottom dead center (BDC). At full compression, the volume of the combustion chamber above the piston has a substantially constant (and minimum) volume during only a small portion of the angular rotation of the crank. Particularly at high crank rotation rates, this is an insufficient interval to provide complete combustion of the fuel at a constant volume.

In applicant's previous apparatus described in the application noted above, complete constant volume combustion is achieved with a connecting rod that provides added distance between the crank and the piston as the connecting rod is pivoted with respect to the piston. Effectively, the rod pushes the piston away as the crank pivots the rod past TDC, with the pushing away serving to counteract for a time the initial downward motion of the piston. This is achieved by a curvilinear cam groove engaged by a pin on the piston. The net effect provides constant volume combustion by combining a small cyclical vertical motion of the piston relative to the connecting rod with the conventional sinusoidal motion of the piston. As a result, the normal sinusoidal peaks of a conventional engine are flattened and extended to form plateaus; as the piston pauses or dwells without substantial downward motion for a time after the crank passes TDC. During this period, the combustion chamber volume is substantially constant. These plateaus have a sufficient width, that is, the piston dwell time after TDC is sufficient for the fuel mixture to be entirely burned.

Although the prior art apparatus is effective to provide fuel efficient and clean combustion, particularly with two-stroke engines, it has several functional limitations:

A first limitation of the prior art apparatus is that it is susceptible to wear, particularly at the cam groove. Substantially all of the explosive force of the engine is transmitted to the crank shaft by a pin on the piston that engages the cam groove. The high frictional

- 3 -

loading pressures at this interface causes unavoidable wear that eventually degrades performance and decreases life expectancy.

A second limitation of the prior art apparatus is the high manufacturing cost needed to maximize the wear-resistance of the components. To get maximum life expectancy from the connecting rod crank, the forged rod must be cut, ground and polished at the cam groove. These multiple manufacturing steps increase manufacturing costs. In addition, the cam groove has a particular irregular shape to provide the proper piston motion profile. This shape requires precise machining to give optimum performance.

A third limitation of the prior art apparatus is that a single connecting rod cam groove design achieves only a single piston motion profile. Therefore, if the engine is to be converted to an alternative fuel, new connecting rods must be designed, manufactured and installed. In addition, for a single fuel, the piston motion profile must be selected to provide an adequate compromise of performance at various crank shaft rotation rates. A profile optimized for slower rotation rates may not achieve constant volume combustion at higher rotation rates because the increased angular velocity of the crank shaft affords less actual time at constant volume for the fuel to burn. A profile optimized for high RPMs may result in excessive dwell that increases internal mechanical stresses and impairs efficiency.

30 SUMMARY OF THE INVENTION

The primary object of the invention is to provide an improved adjustable length connecting rod for an internal combustion engine, providing prolonged periods of substantially constant combustion chamber volume with long-wearing components.

It is a further object to provide a connecting rod as aforesaid that may be further adjusted to provide

- 4 -

extended or reduced periods of constant volume combustion to optimize performance at a wide range of engine speeds.

It is yet another object of the invention to provide a connecting rod as aforesaid that is adjustable to accommodate a variety of fuels having different combustion properties while maintaining the advantages of constant volume combustion. The preferred embodiment of the invention includes several features which act independently and cooperatively to achieve the above objects.

According to the present invention, the objects are achieved by providing a connecting rod between a crank shaft and a piston. The piston end of the crank shaft defines a sleeve in which a disc having an eccentric bore is rotatably mounted. The eccentric bore receives a wrist pin on which the piston pivots. A disc shifter bar is pivotally connected to a second eccentric position on the disc at one end of the bar and slidably connected at the other end to a pin mounted to an intermediate portion of the connecting rod. An intermediate portion of the shifter bar is longitudinally slotted to receive slidably a second stationary pin on the piston. Consequently, angular displacement of the connecting rod with respect to the piston rotates the disc to extend or retract the piston relative to the connecting rod.

The invention may further include a compensator to shift any one of the attachment pins to change the shifting geometry of the mechanism, thereby optimizing the invention for alternate fuels or a range of engine speeds. The invention may further include the remaining components of an engine, including a controller for remotely adjusting the compensator in response to changes in engine speed or fuel composition.

The foregoing and additional features and advantages of the present invention will be more readily apparent from the following detailed description which proceeds with reference to the accompanying drawings.

- 5 -

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a sectional side view of a piston and connecting rod according to the present invention.

FIG. 2 is a sectional side view of the apparatus
5 of FIG. 1 taken along line 2-2.

FIG. 3 is a fragmentary sectional side view of an alternative embodiment of the apparatus of FIG. 1 showing a pin adjustment mechanism.

FIG. 4 is a sectional side view of the apparatus
10 of FIG. 1 with the crank rotated partially past top dead center.

DETAILED DESCRIPTION OF A PREFERRED EMBODIMENT

FIG. 1 shows a connecting rod assembly 10 for
15 connecting a crank shaft 68 and a conventional piston 12 arranged to reciprocate in a cylinder 74 defined in a conventional two-stroke or four-stroke internal combustion engine 76. Alternatively, the assembly may be employed in a compressor, pump, refrigeration device or the like,
20 using similar mechanisms. In some such alternative applications, such as a fuel injector, the disclosed apparatus may be modified to produce a reduced dwell for a pumping impulse instead of a pause at top dead center.

The connecting rod assembly includes a unitary
25 forged connecting rod 16 having an upper end 18 defining a cylindrical sleeve 20. A cylindrical disc 22 is closely and rotatably received within the sleeve 20. The disc defines a wrist pin bore 26 offset from and parallel to the axis of the disc, passing entirely through the disc to
30 closely and rotatably receive a wrist pin 28, which is rigidly mounted within the piston, as shown in FIG. 2.

As further shown in FIG. 2, a rigid, elongated shifter bar 32 is pivotally mounted at an upper end 34 to an eccentric point 36 on the disc 22. The eccentric point
35 36 is the axial center of an eccentric bore 40 defined in the disc 22 at a position offset from the center of the disc and angularly offset about the center of the disc from the wrist pin bore 26. The angular offset may be of

any value, with 0 degrees providing a mildly increased dwell centered at TDC, 90 degrees providing substantial dwell after TDC, 180 degrees providing mildly decreased dwell at TDC, and 270 degrees providing dwell before TDC, with intermediate values providing intermediate results. In the preferred embodiment, 80 degrees has been selected to provide the desired dwell after TDC. When a mild dwell is desired, the shifter bar may be attached directly to the wrist pin to provide a 0 degree offset angle.

10 The shifter bar 32 includes a disc shifter pin 42 sized to be rotatably received in the eccentric bore 40. At an intermediate position 46 on the shifter bar 32, the shifter bar defines an elongated piston pin slot 48. The piston pin slot 48 is centrally aligned along the length of the shifter bar 42 and is sized to slidably receive a piston pin 50 that protrudes inwardly from the interior of the piston 12. The piston pin 50 is oriented on an axis parallel to the wrist pin 28 at a position well below the wrist pin and slightly laterally offset therefrom.

20 The shifter bar 32 includes a lower end 54 defining a lower slot 56 configured similarly to the piston pin slot 48 and sized to slidably engage a rod pin 58 fixed to and protruding from the connecting rod 16 at an intermediate position thereon. The connecting rod 16 defines at its lower end 60 a crank sleeve 64 sized to rotatably receive an orbiting portion of the crank 68.

EXAMPLE

In a preferred embodiment engine, the piston has a diameter of 80 mm and a stroke of 137 mm. The stroke corresponds to the diameter of the circle traced by the center of the orbiting crank portion within the crank sleeve 64. The illustrated embodiment is optimized for operation at 9,000 rpm, providing a dwell time of substantially constant volume combustion for approximately 15 degrees after top dead center, in a two-stroke engine using gasoline. This dwell angle may be any amount up to about 20 degrees, depending on fuel, speed, and

- 7 -

application. As illustrated, the wrist pin 28 has a diameter of 5 mm and the disc shifter pin 42, the piston pin 50 and the rod pin 58 are each 4 mm in diameter. The disc 22 has a diameter of 1 inch, with the center of the wrist pin bore 26 being offset from the center of the disc by 7 mm. The eccentric bore 40 is similarly offset from the center of the disc by 7 mm and is angularly offset from the wrist pin bore 26 by 80 degrees in a clockwise direction. The piston pin 50 is vertically offset below the wrist pin 28 by 2.854 inches and laterally offset by 7 mm, an amount corresponding to the eccentric offset of the wrist pin bore 26. The rod pin 58 is spaced below the center of the disc by $5\frac{1}{2}$ inches, or half the 11 inch overall center-to-center length of the connecting rod 16. Positioning the rod pin substantially below this location may cause interference with a conventional crank shaft when the piston is at bottom dead center. The sleeve 64 has a diameter of 2 inches. The shifter bar has a thickness of $\frac{3}{16}$ inches and a width of $\frac{1}{2}$ inch, with the slots 48 and 56 being sufficiently elongated to accommodate the relative motion of the components.

To provide optimization for various fuels, engine sizes and speeds, numerous dimensions may be adjusted to control the angular period during which the piston dwells after top dead center. To increase the dwell time, any number of changes may be made: the disc shifter pin 42 may be moved closer to the center of the disc, the wrist pin bore 26 may be offset farther from the center of the disc 22, the rod pin 58 may be moved upward toward the disc, the piston pin 50 may be moved downward away from the disc, and the angular offset between the wrist pin bore 26 and the eccentric bore 40 may approach 90 degrees. The dwell angle may be reduced by making the corresponding opposite adjustments. Note, however, that for a given stroke or crank orbit diameter, the eccentric point 36 must be adequately offset in the disc 22 to allow the disc shifter pin 42 on the shifter bar 32 to sweep through its full range of motion as the lower end 60 of the connecting

- 8 -

rod 16 makes a complete orbit. Where the eccentric point is inadequately offset, the crank orbit diameter must be suitably reduced.

In an alternative embodiment shown in FIG. 3, a compensator may be provided to adjust the piston dwell period while the engine is operating. This adjustment will compensate for variations in engine speed or fuel combustion properties. In this embodiment, the rod pin 58, or alternatively the piston pin 50, or any other geometrically critical component may be adjusted selectably to optimize the engine for alternative fuels and speeds. An adjustment mechanism 82 includes a vertically adjustable rod pin 58 that slides in a groove 84 defined in the connecting rod 16. A remotely controlled solenoid 86 or other linear actuator is connected to the pin 58 to adjust its position. This provides the advantage of optimizing the piston motion profile and dwell period during operation of the engine. Thus, the pin may be shifted to an optimal position as a function of engine speed. The slidable pin may be controlled over a continuously variable range of positions or may be toggled between two separate positions, each suitable for a range of operating conditions. The toggle mode may also be used to convert an engine to an alternative fuel having different combustion characteristics.

In another alternative embodiment, a sensor may detect the properties of an unknown fuel mixture so that a controller may adjust the appropriate position of the shiftable pin. Similarly, other sensors such as exhaust gas analyzers and temperature sensors may detect evidence in the exhaust gas of incomplete combustion, permitting the controller to adjust the dwell time, thereby optimally tuning the engine as it operates.

35

OPERATION

FIG. 4 illustrates the operation of the connecting rod assembly 10 as a crank arm 68 attached to the crank sleeve 64 rotates through an initial crank angle

- 9 -

70 illustrated as 15 degrees past top dead center. For comparison, FIG. 1 shows the assembly at top dead center. The piston 12 is shown in a cylinder 74 defined in an engine block 76. A combustion chamber 78 defined within the cylinder 74 by the upper face of the piston remains at substantially constant volume between the top dead center position shown in FIG. 1 and the position shown in FIG. 4.

As further shown in FIG. 4, the generally leftward motion of the lower end 60 of the connecting rod 16 causes the lower end of the shifter bar 32 to move leftward at the rod pin 58. Because the piston pin 50 is fixed to the piston 12 and does not move laterally, it provides a fulcrum about which the shifter bar pivots. Consequently, the upper end 34 of the shifter bar 32 moves to the right, with this rightward motion being accommodated by a counterclockwise rotation of the disc 22. This counterclockwise rotation initially causes the wrist pin 28 to move upward relative to the connecting rod 16. Because the connecting rod is drawn generally downward by the rotation of the crank arm 68, this upward motion of the wrist pin 28 effectively cancels the downward motion so that the wrist pin and piston remain essentially stationary while the connecting rod moves downward. With the effective length of the connecting rod being the center-to-center distance between the wrist pin bore 26 and the crank sleeve 64, the effective length is adjusted to provide the desired constant volume combustion.

Having illustrated and described the principles of my invention with reference to a preferred embodiment, it should be apparent to those skilled in the art that the embodiment may be modified without departing from such principles. For instance, the invention may be employed in two-stroke or four-stroke or other engines employing any of a wide variety of fuels, or may be employed in any reciprocating piston machine such as a compressor or pump. I claim as my invention all such modifications as come within the true spirit and scope of the following claims.

- 10 -

I claim:

1. A connecting rod assembly for connecting a crankshaft and a piston, comprising:
 - a first end portion operably connected to the
5 crankshaft,
 - a second end portion operably connected to the piston, the second end portion defining a sleeve,
a disk rotatably received in the sleeve, the disk
defining an eccentric bore for receiving a portion of the
10 piston such that the rod may pivot on the axis of the bore
with respect to the piston, and
a disc shifter operably connected to the disk for
rotating the disk such that the disk rotates in
conjunction with pivoting between the rod and the piston.
15
2. The connecting rod assembly of claim 1
wherein the disk shifter is operably connected to the rod
and the piston.
- 20 3. The connecting rod assembly of claim 1
wherein the disk shifter interacts with the disk at an
eccentric point on the disk.
4. The connecting rod assembly of claim 3
25 wherein the eccentric point is angularly offset about the
center of the disk from the center of the eccentric bore.
5. The connecting rod assembly of claim 4
wherein the angular offset is between 0 and 180 degrees.
30
6. The connecting rod assembly of claim 1
wherein the disk shifter comprises a rigid elongated
member having a first end operably connected with the
disk, a second portion operably connected to the piston,
35 and a third portion operably connected to the connecting
rod.

- 11 -

7. The connecting rod assembly of claim 6 wherein the shifter first end is pivotally attached to the disk, the second portion is slidably connected to the piston, and the third portion is slidably connected to the
5 connecting rod.

8. The connecting rod assembly of claim 6 wherein the second portion is intermediate the first end and the third portion.
10

9. The connecting rod assembly of claim 6 wherein the second portion of the shifter is slidably and pivotally connected to the piston.

10. The connecting rod assembly of claim 6 wherein the third portion of the shifter is slidably and pivotally connected to an intermediate portion of the connecting rod.
15

11. A method of operating a piston attached to a crankshaft by a connecting rod comprising the steps:
rotating the crankshaft,
cyclically with rotation of the crankshaft
sliding the piston between a top position remote from the
crankshaft and a bottom position proximate the crankshaft,
25 and

cyclically with rotation of the crankshaft
adjusting the effective length of the connecting rod such that the piston remains substantially motionless during a
30 portion of crankshaft rotation.

12. The method of claim 11 wherein the piston is held substantially motionless when the piston is near the top position.
35

13. The method of claim 11 wherein the piston is held substantially motionless during between 4 and 20 degrees of crankshaft rotation.

- 12 -

14. The method of claim 11 wherein the
connecting rod includes a first rod end having a rotatable
disk having an eccentric attachment point, and a second
5 rod end opposite the first rod end, and

wherein the step of adjusting the effective
length comprises rotating the disk such that the eccentric
attachment point is variably spaced apart from the second
rod end.

10

15. A reciprocating piston apparatus comprising:
a piston,
a crankshaft, and
an adjustable connecting rod operably connected
15 at a first end connection to a first portion of the
piston, and at a second end connection to the crankshaft,
the distance between the first and second end connections
being cyclically adjustable with rotation of the
crankshaft such that the piston remains substantially
20 stationary during a period of crankshaft rotation.

16. The apparatus of claim 15 wherein the
connecting rod first end includes a sleeve for receiving a
disk defining an eccentric bore forming the first end
25 connection, such that rotating the disk adjusts the
distance between the first and second end connections.

17. The apparatus of claim 15 wherein the
connecting rod is operably connected at a third connection
30 to a portion of the piston.

18. The apparatus of claim 17 wherein at least
one of the first end connection, the second end connection
and the third connection is selectably movable to adjust
35 the period of crankshaft rotation during which the piston
remains substantially stationary.

- 13 -

19. The apparatus of claim 17 including a controller operably to the selectably movable connection to adjust the movable connection as a function of crankshaft rotation.

5

20. The apparatus of claim 17 including a selector for selecting between at least two positions of the movable connection to accommodate different fuels having different combustion properties.

10

21. A multiple-fuel engine suitable for burning fuels having different combustion properties comprising:

a cylinder,

a piston defining with the cylinder a chamber,

15

a rotatable crankshaft,

a connecting rod operably connecting the piston to the crankshaft,

an adjusting mechanism for cyclically with rotation of the crankshaft adjusting the effective length of the connecting rod to maintain the chamber at a substantially constant volume during a period of crankshaft rotation, and

20

a fuel compensator operably connected with the adjusting mechanism for selectably changing the period of crankshaft rotation during which the chamber is maintained at a substantially constant volume.

25

22. The engine of claim 21 wherein the adjusting mechanism includes a shifter bar operably connected to the connecting rod and piston at connection points, and wherein the compensator comprises an actuator to move at least one of the connection points.

30

23. The engine of claim 22 wherein the compensator comprises a solenoid.

35

24. A reciprocating piston apparatus comprising:
a piston.

- 14 -

a crankshaft,

a connecting rod operably connected at a first end connection to a first portion of the piston, and at a second end connection to the crankshaft, and

5 adjustment means for cyclically adjusting the distance between the first and second end connections of the connecting rod with rotation of the crankshaft, such that the piston remains substantially stationary during a first period of crankshaft rotation.

10

25. The apparatus of claim 24 including compensator means operably connected to the adjustment means for changing the cyclical adjustment such that the piston remains stationary during a second period of
15 crankshaft rotation different from the first period.

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FIG. 1

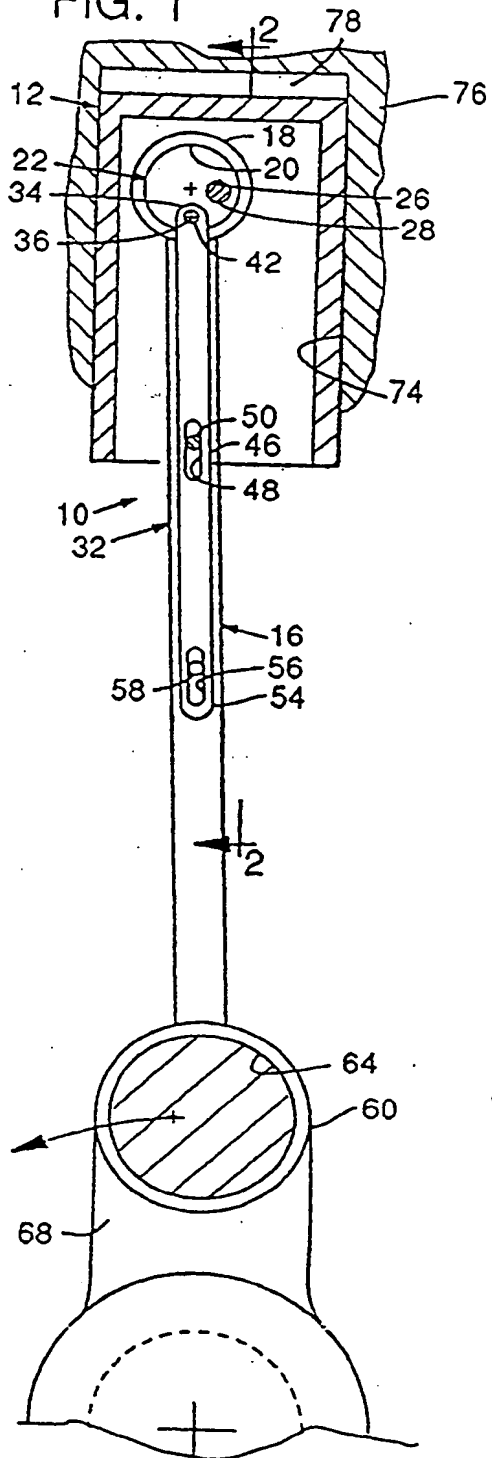
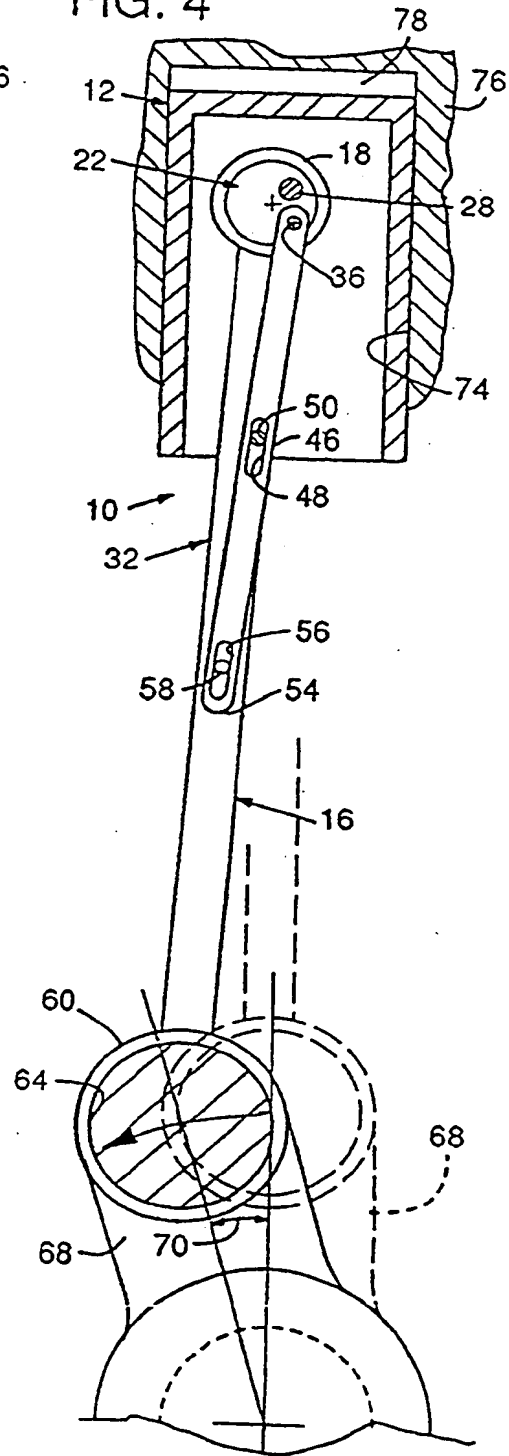


FIG. 4



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FIG. 2

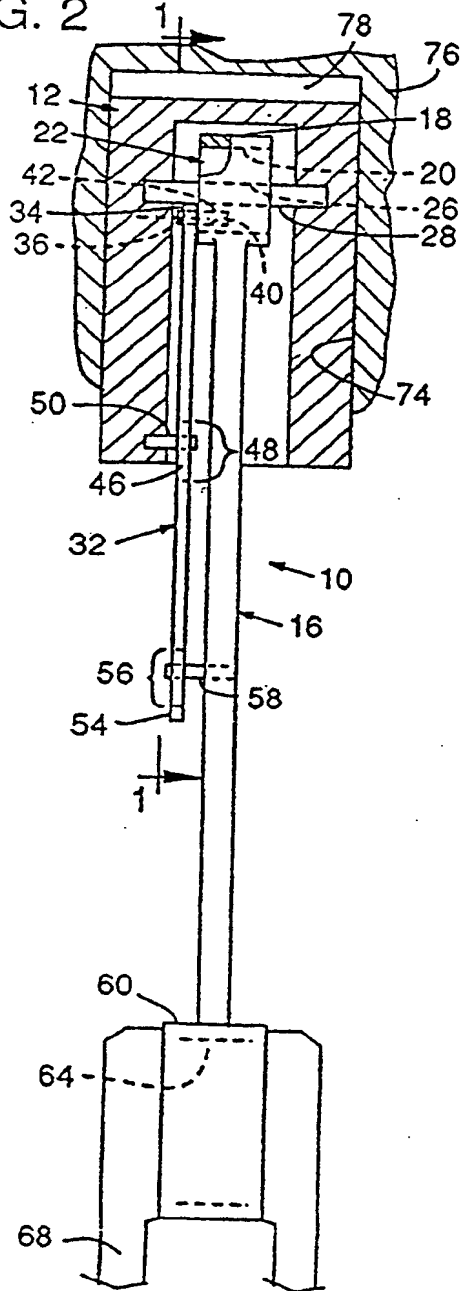
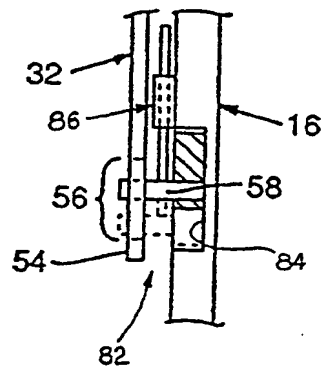


FIG. 3



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US93/08811

A. CLASSIFICATION OF SUBJECT MATTER

IPC(5) : F02B 75/32

US CL : 123/197.3; 92/187; 74/579E

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 123/197.3, 48B, 78E, 197.1, 197.4; 92/140, 187; 74/40, 44, 579E, 579R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US, A, 1,518,334 (McMaster) 09 December 1924, page 2, lines 66-97.	11, 12, 14, 15, 17, 24
X	DE, A, 3,444,233 (Hulsmeyer) 05 June 1986, abstract.	11, 12, 13
A	US, A, 4,485,768 (Heniges) 04 December 1984.	1-25
A	US, A, 1,873,908 (Schinke) 23 August 1932.	1-25
A	US, A, 3,633,429 (Olson) 11 January 1972.	1-25
A	DE, A, 3,233,314 (Lehr) 08 March 1984.	1-25
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